

**A SPOOL WITH SUBSTANTIALLY TEMPERATURE INSENSITIVE HUB AND A  
METHOD OF MAKING SAME**

**BACKGROUND OF THE INVENTION**

**CROSS-REFERENCE TO RELATED APPLICATIONS**

[0001] This application claims the benefit of U.S. Provisional Application Serial No. 60/466668, filed April 30, 2003, entitled "A Spool with Substantially Temperature Insensitive Hub and a Method of Making Same."

**FIELD OF THE INVENTION**

[0002] The present invention relates generally to spools for holding optical fiber, and particularly to spools for holding dispersion compensating fiber.

**TECHNICAL BACKGROUND**

[0003] Optical signals transmitted in an optical fiber transmission system typically constitute a series of pulses. Although, within each channel, the pulses are usually centered at a single nominal wavelength, each pulse is actually composed of different spectral components. These spectral components propagate through transmission or typical amplification fibers at different speeds (due to a phenomena referred to as chromatic dispersion). This can result in spectral components of one pulse arriving at a receiver at the same time as the succeeding pulse, thereby degrading the signal to noise ratio. Thus, optical fiber communication systems utilize dispersion compensating modules ("DCM"), to correct for chromatic dispersion. A typical dispersion compensating module includes a housing with one or more spools 10 of dispersion compensating fiber (DCF). This dispersion compensating fiber offsets the chromatic dispersion produced in the transmission and/or amplification fiber. This approach is disclosed, for example, in US patent number 6,456,773 and is illustrated in **Figure 1**.

[0004] A typical spool **10** of DCF is shown in **Figure 2** and includes a cylindrical hub **12**, two flanges **14**, **14'**, a cover plate **16** and a protective casing **18**. The casing **18** covers the fiber and is situated between the flanges. The DCF is wound around the hub **12** between the two flanges **14**, **14'** and is protected by the casing **18**. The dispersion compensating fiber typically enters into the spool via the underlay groove **15** provided on the internal surface of one of the flanges and exits the spool via the fiber exit or fiber reverse groove **20**, provided on the external surface of one of the flanges. The underlay groove **15** is utilized to get the DCF to the hub **12**, so as to enable the startup of the winding process. The underlay groove **15** is tangential to the outer diameter of the flange in order to minimize fiber bending. However, this ties the geometry of the underlay groove to the required form factor (i.e., overall size and shape of the package).

[0005] After winding is completed, the dispersion compensating fiber exits the spool **10** via the fiber groove **20**. In order to protect this fiber a cover plate **16** is then fitted over the external surface (the surface not in contact with the hub **12**) of the flange **14'** (and the dispersion compensating fiber contained within the fiber groove **20**). In order to minimize fiber bending, and in order to maximize mechanical reliability and life span of DCF, the fiber groove **20** is positioned to allow the DCF to exit substantially tangentially to the radius of the flange. In non-round packages, a mandrel in the box typically reverses the direction of the exiting fiber to align it with fiber entry orientation. In a round package this is done by the reversing fiber groove **20**, so that both entering fiber and exiting fiber points in the same direction.

[0006] The dispersion fiber containing spools have to be custom made for each customer because each customer requires a different size spool. For example, because the fiber underlay and fiber grooves terminate tangentially to the radius of the flange, the flanges can not be cut down to a smaller size. Thus, features of the plain flange **14**, the grooved flange **14'** and the casing **18** are dependent on the required form factor.

[0007] The hubs of the spools are typically molded for different thicknesses. The molded parts are then machined to different sizes to maximize the fiber holding capacity for a given form factor. Because the form factor is customer dependent, a standard size hub can not be used. This further increases the cost of the DCM spools.

[0008] In addition, if the thermally induced expansion of the hub exceeds a certain value, the DCM turns dark (i.e., stops functioning). Thus, because wound DCF is sensitive to temperature induced stress and has a low coefficient of thermal expansion (CTE), the hubs are usually made from materials with low CTE, for example Macor<sup>TM</sup>, Invar<sup>TM</sup>, or Covar<sup>TM</sup>. During temperature fluctuations, this allows the wound DCF to expand at about the same rate as the hub, minimizing fiber stretching. Macor<sup>TM</sup> is a glass ceramic with CTE which is similar to that of the DCF. However, it is a very expensive material. Invar<sup>TM</sup> and Covar<sup>TM</sup> have a higher CTE than Macor, and are also very expensive.

#### SUMMARY OF THE INVENTION

[0009] One aspect of the invention is a spool comprising: a hub sandwiched between two flanges at least one of said flanges including at least one smoothly curving arcuate fiber groove on a side facing said hub, said fiber groove extending substantially to the outer edge of said flange, said groove being at an angle  $\theta$  relative to the tangent line to the periphery of said flange.

[0010] Additional features and advantages of the invention will be set forth in the detailed description which follows, and in part will be readily apparent to those skilled in the art from that description or recognized by practicing the invention as described herein, including the detailed description which follows, the claims, as well as the appended drawings.

[0011] It is to be understood that both the foregoing general description and the following detailed description present embodiments of the invention, and are intended to provide an overview or framework for understanding the nature and character of the invention as it is claimed. The accompanying drawings are included to provide a further understanding of

the invention, and are incorporated into and constitute a part of this specification. The drawings illustrate various embodiments of the invention, and together with the description serve to explain the principles and operations of the invention.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

- [0012] Figure 1 illustrates a Prior Art spool suitable for holding a DCF;
- [0013] Figure 2 illustrates a construction of a spool of DCF according to Prior Art;
- [0014] Figure 3 is a exploded view of a DCM according to of one embodiment of the present invention;
- [0015] Figure 4 illustrates a first embodiment of an exemplary hub utilized in a DCM;
- [0016] Figure 5 illustrates a second first embodiment of an exemplary hub utilized in the DCM;
- [0017] Figure 6 illustrates an embodiment of an extruded hub pipe that is cut to a required size to provide a hub of length l;
- [0018] Figure 7 illustrates a first embodiment of a stamped universal flange preform;
- [0019] Figure 8 illustrates an exemplary strip of flange preforms and a resultant flange, after it has been trimmed to size;
- [0020] Figure 9 illustrates another first embodiment of a flange;
- [0021] Figure 10 illustrates a fiber groove that allows the fiber to exit in a direction opposite from the entering direction.

### **DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS**

[0022] Reference will now be made in detail to the present preferred embodiments of the invention, examples of which are illustrated in the accompanying drawings. Whenever possible, the same reference numerals will be used throughout the drawings to refer to the same or like parts. One exemplary embodiment of the DCF spool of the present invention is shown in **Figure 3**, and is designated generally throughout by the reference numeral **100**.

[0023] As embodied herein and depicted in **Figure 3** the spool **100** includes a hub **112** and two flanges **114A**, **114B** and, does not require a cover plate. Preferably, the hub **112** is made from a relatively inexpensive material, such as aluminum or inexpensive plastics, for example Propylux<sup>TM</sup> FR, available from Westlake Plastics, Lenni, PA. The hub **112** is constructed in a manner that would substantially (less than 0.1%) preserve hub's outer diameter  $D_H$  during temperature fluctuations, thus minimizing  $D_H$  changes. It is preferred that the hub's outer diameter  $D_H$  changes by less than preferably 0.05% and most preferably by less than 0.035% of its diameter during the temperature variations between  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ . The hub **112** is designed to transform what would otherwise be radial expansion induced by the change in temperature (from  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ ) into tangential displacement. This allows one to eliminate the use of very expensive materials with a very low coefficient of thermal expansion for manufacturing the hub. Two exemplary designs of hubs of the present invention are illustrated in **Figures 4** and **5**.

[0024] More specifically, **Figure 4** illustrates a cross sectional view of the first exemplary hub embodiment. The hub **112** of this embodiment includes at least one "living" hinge **113** forming a cavity in the periphery of the hub. The hinge **113** includes a narrow gap or an opening **113A** in the outer (cylindrical surface) of the hub **112** and a bridge **113B**. When the temperature increases, the outer surface circumference of the hub **112** increases, without increasing the outer diameter  $D_H$  of the fiber barring surface, thereby closing or reducing the size of the gap **113A**. When the temperature decreases, the outer surface circumference of the hub **112** decreases, without decreasing the outer diameter  $D_H$  of the fiber barring surface (the outer diameter of the hub **112**), thereby enlarging the gap **113A**. The hub **112** also includes optional structural ribs **113C**. These ribs add strength to the hub **112** and provides support for the rivets for attachment to the flanges **114A** and **114B**. If the hub is made of metal, for example, aluminum, the ribs may not be needed.

[0025] **Figure 5** illustrates a cross sectional view of the second exemplary hub embodiment. The hub **112** of this embodiment includes at a plurality of "living" hinges **113**. In this design, in order to maintain outer diameter of the fiber bearing surface of the

hub, utilizes openings **113A** in the circumference and surface folds **113B**. When the temperature increases, the length *L* of the fiber bearing sections located between the openings **113A** increases, narrowing these openings, without increasing the outer diameter of the fiber bearing surface. In addition, the fold surfaces **113B** provide structural strength to the hub **112** and can be used to hold the rivets that attach the hub **112** to the flanges **114A**, **114B**.

[0026] In order to minimize manufacturing costs, it is preferable that the hub **112** be made with material that has a relatively large CTE, for example  $14\mu\text{in/in } ^\circ\text{C}$  or higher, and more preferably  $20\mu\text{in/in } ^\circ\text{C}$  or higher, at the temperature range of  $-40^\circ\text{C}$  to  $85^\circ\text{C}$ . It is preferable that the hub be made from an inexpensive plastic suitable for extrusion. As illustrated in **Figure 6**, an extruded hub pipe **112A** can be cut, as needed, to a size specified by the end user, further minimizing manufacturing costs. Examples of some of the suitable materials are provided in Table 1, below.

**Table 1**

| Material       | CTE ( $\mu\text{m} / \text{in } ^\circ\text{C}$ ) | Modulus (ksi)     | CTE*Modulus        | Relative Cost |
|----------------|---|-------------------|--------------------|---------------|
| Ultem® 2300    | 11  | $900 \times 10^3$ | $9.9 \times 10^6$  | \$\$\$\$      |
| Hydex™ 6120    | 14  | $900 \times 10^3$ | $12.6 \times 10^6$ | \$\$\$        |
| Zelux™ M       | 38  | $340 \times 10^3$ | $12.9 \times 10^6$ | \$\$          |
| Lexan® 943     | 38  | $325 \times 10^3$ | $12.3 \times 10^6$ | \$\$          |
| Cyclooy® C2950 | 40  | $385 \times 10^3$ | $15.4 \times 10^6$ | \$\$          |
| Propylux™      | 21  | $220 \times 10^3$ | $4.6 \times 10^6$  | \$            |

|    |  |  |  |  |
|----|--|--|--|--|
| FR |  |  |  |  |
|----|--|--|--|--|

**[0027]** The materials Ultem®, Lexan® and Cycloy® are commercially available from GE Plastics, of Schenectady, NY. The materials Zelux™ and Propylux™ are commercially available from West Lake Plastics of Lenni, NY. Hydrex™ is are commercially available from A. L. Hyde Company of Grenloch, NJ.

**[0028]** In accordance with one embodiment of the invention, a method of making a spool **100** for DCF includes the following steps: extruding a plastic hub pipe **112A** having at least one living hinge **112A'**; cutting off a required length  $l$  of this hub pipe **112A**, thereby producing a plastic hub **112** of length  $l$ , the hub **112** having at least one living hinge **113**; providing two flanges **114A**, **114B**; assembling the plastic hub **112** and the flanges **114A**, **114B** into a spool **100**. As stated above, in order to minimize manufacturing costs, it is preferable that less expensive plastics be used. These plastics have CTE  $14\mu\text{in/in } ^\circ\text{C}$  higher, and more preferably  $20\mu\text{in/in } ^\circ\text{C}$  or higher, at the temperature range of  $-40^\circ\text{C}$  to  $85^\circ\text{C}$ .

**[0029]** In accordance with another embodiment of the invention, a method of making a spool **100** for DCF includes the following steps: producing a metal hub pipe **112A**, cutting a required length of this hub pipe **112A**, thereby producing a hub **112**; providing two flanges **114A**, **114B**; assembling the hub **112** and said flanges **114A**, **114B** into a spool **110**. An aluminum hub pipe may be produced, for example, by extrusion.

**[0030]** Thus, according to an embodiment of the present invention a spool comprises a hub **112** sandwiched between two flanges **114A**, **114B**. The hub contains at least one living hinge forming a cavity in a periphery of said hub, such that during the temperature variations between  $-40^\circ\text{C}$  to  $85^\circ\text{C}$ : (i) the outer surface circumference of the hub changes, thereby changing the size of the opening associated with the cavity; and (ii) the outer surface diameter  $D_H$  of said hub remains substantially constant.

**[0031]** The flanges **114**, **114B** can be made from either metal, for example aluminum or steel, or plastic. Preferably, the features of the flanges **114A**, **114B** are independent of the

flange diameter, allowing for less expensive manufacturing. The flanges **114A**, **114B** are preferably made by first stamping out a universal flange preform **114** (shown in **Figure 7**) and then trimming the stamped flange preform **114** to an outer diameter  $D_F$  on as needed basis. By this method, identical flange preforms will be used to prepare different diameter flanges for different consumers. According to one embodiment of the present invention a spool comprises: a hub **112** sandwiched between two flanges **114A**, **114B**. At least one of these flanges includes at least one smoothly curving fiber groove **120A** on a side facing the hub. The fiber groove is formed on a surface of the flange and does not extend all the way through the thickness of the flange. The fiber groove **120A** extends substantially (0.0 to 3mm and preferably 0.0 to 2.5mm) to the outer edge of the flange. The fiber groove is arcuate (forms an arc) and forms an angle  $\theta$  relative to the tangential line to a periphery of the flange. It is preferable that the angle  $\theta$  be no more than 15 degrees. It is more preferable that  $\theta$  is less than 10 degrees, even more preferable that  $\theta$  is less than 5 degrees, and most preferable that  $\theta$  is less than 3 degrees. It is preferred that the minimum arc radius of the fiber groove is greater than 20mm and preferably greater than 25mm. The fiber groove is v-shaped and is between 0.030" and 0.045" deep and the size of the groove opening  $w$  is 0.06" to 0.15" and preferably between 0.6" and 0.12". It is most preferable for the groove width to be between 0.7" and 0.1". In this embodiment the groove width is 0.9".

[0032] More specifically, **Figure 7** illustrates that the flange preform **114** includes a plurality of fiber grooves **120A**, **120B**, **120C**, and **120D**. Flange preform **114** may have a larger or a smaller number of the fiber grooves. Each of these fiber grooves **120A**, **120B**, **120C**, **120D** corresponds to a flange with a different range of diameters  $D_F$ . The fiber grooves **120A**, **120B**, **120C**, **120D** are curved such that when flanges are cut to a flange of the desired diameter  $D_F$ , the shape at least one of the fiber grooves would allow (i) the fiber to exit the flange at a shallow angle, preferably parallel to the circumference of the flange **114A**, **114B** and, (ii) the fiber bend radius to be larger than the minimal acceptable bend radius (i.e., at least 20mm). In this embodiment the fiber grooves **120A**, **120B**, **120C**,



**120D** are semicircular, but they may be of another, arcuate, smoothly curving shape. The fiber grooves **120A**, **120B**, **120C**, **120D** are formed on the surface of the flange and do not extend all the way through the thickness of the flange. The fiber grooves **120A**, **120B**, **120C**, **120D** allow the exiting fiber to point in the same direction as the in-coming fiber, so that two fiber ends are spliced to pigtails that are roughly parallel to one another. This feature is advantageous because in packages with circular footprint both the pigtails are managed by the same routing approach. In noncircular packages this feature also eliminates the use of a turn-around mandrel. However, the fiber grooves can be modified to provide an option of fiber exiting in a direction opposite of direction of entry. The exiting fiber can be spliced to pigtails by means known in the art.

[0033] The fiber grooves **120A**, **120B**, **120C**, **120D** are characterized by their respective radii  $R_A$ ,  $R_B$ ,  $R_C$ ,  $R_D$ , wherein  $R_A < R_B < R_C < R_D$ . The smaller radii correspond to the smaller diameter flanges and the larger radii correspond to the larger diameter flanges. For example, the fiber groove **120A** corresponds to the flanges with the diameter  $D_F$ , where  $D_F' < D_F < D_F''$ . This is shown, for example, in **Figure 7**, which illustrates that groove **120A** may be used for all form factors that have diameters between two circles shown by dashed circles. The spacing between the dashed circles depends on the required clearance between the end of the wound fiber and the flange perimeter, so as to allow adequate space for splices and pigtails. A typical distance between perimeter of the wound fiber and the perimeter of the flange is 3 to 5mm (assuming maximum amount of wound fiber). In this embodiment the groove exits tangent to the average diameter of the dashed circles. More specifically, groove **120A** characterized by a radius of curvature  $R_a=25\text{mm}$  corresponding to  $195\text{mm} < D_F < 200\text{mm}$ . An exemplary strip of flange preforms and a resultant flange trimmed to a desired diameter are illustrated in **Figure 8**.

[0034] Preferably, fiber grooves are placed on the internal side of the flange -i.e., the side facing the hub. This placement of fiber grooves is illustrated in **Figure 3** and eliminates the need for an external cover plate. In addition to the fiber grooves, one of the flanges, for example **114B**, may include a notch **115** for identifying the desired groove. This notch can

be easily provided during the trimming process. In addition, this notch **115** helps in retaining one end of the fiber during the winding process. More specifically, if the fiber groove does not reach the periphery of the flange, the notch **115** on the flange periphery brings the groove to the edge of the flange.

[0035] Another embodiment of the flange **114** is illustrated in **Figures 9 and 10**. This flange includes 2 grooves. Groove A is a reversing groove. It allows the fiber leads exit in the same direction. The fiber exits at shallow angles and the same groove accommodates flanges of different diameters. **Figure 10** illustrates a smaller diameter flange that was trimmed (to a smaller diameter) from an identical preform that trimmed to provide the flange of **Figure 9**. Groove B allows the fiber to exit in a direction opposite from the entering direction (i.e., the fiber leads point to different directions). This is illustrated in **Figure 10**. The advantage is that this flange design can be used to provide a wide range of flange diameters. For example, it has been utilized to provide flanges with outer diameters between 190mm and 300mm. An ability to derive flanges of any outer diameter from one flange preform advantageously reduces manufacturing costs and results in shortened lead-time.

[0036] It will be apparent to those skilled in the art that various modifications and variations can be made to the present invention without departing from the spirit and scope of the invention. Thus it is intended that the present invention cover the modifications and variations of this invention provided they come within the scope of the appended claims and their equivalents.